

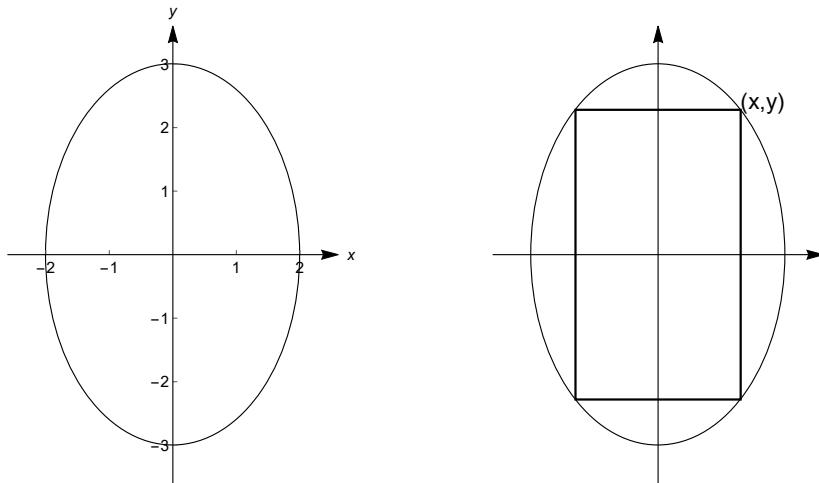
EKSAMEN

Emnekode: IRF30017	Emnnavn: Matematikk 3
Dato: 07.01.2019 Sensurfrist: 28.01.2019	Eksamenstid: 0900-1300
Antall oppgavesider: 3 Antall vedleggsider: 7	Faglærer: Fredrikstad: Mikkel Thorsrud (bortreist) Kontaktperson: Kent Ryne (69 60 87 37). Halden: Einar von Krogh (69608299) Oppgaven er kontrollert: Ja
Hjelpebidrifter: <ul style="list-style-type: none">Godkjent kalkulatorEtt A4-ark med valgfritt innhold (maskin eller håndskrevet, kan skrive på begge sider)Enten Tor Andersen: "Aktiv formelsamling i matematikk" eller "Gyldendals formelsamling i matematikk"	
Om eksamensoppgaven: Oppgavesettet består av 11 deloppgaver som i utgangspunktet vektes likt: 1, 2a, 2b, 3a, 3b, 3c, 4a, 4b, 5a, 5b, 5c. Formelsamling (7 sider) er vedlagt.	
Kandidaten må selv kontrollere at oppgavesettet er fullstendig	



Oppgave 1

- Les av store og lille halvaksen til ellipsen i figuren til venstre. Skriv ned ligningen for ellipsen.
- Figuren til høyre viser et rektangel innskrevet i den samme ellipsen. Bruk Lagranges multiplikatormetode til å finne maksimumsarealet til et rektangel innskrevet i ellipsen. Tips: la hjørnet i første kvadrant ha koordinater (x, y) , se figur. Rektangelets areal og betingelsen kan da uttrykkes ved x og y .



Oppgave 2

- Regn ut dobbeltintegralet

$$\iint_R f(x, y) dA$$

hvor $f(x, y) = 3xy$ og R er trekanten med hjørner i punktene $(0, 0)$, $(4, 0)$ og $(2, 2)$. Hva er middelverdien til funksjonen f over R ?

- Regn ut trippelintegralet

$$\int_0^1 \int_0^{\sqrt{x}} \int_0^y 2e^x dz dy dx$$

Vis alle mellomregninger.

Oppgave 3 En kurve C er gitt ved følgende parametrisering:

$$\mathbf{r} = 3 \sin t \mathbf{i} + 5 \cos t \mathbf{j} + 4 \sin t \mathbf{k}, \quad 0 \leq t \leq \frac{\pi}{2}$$

- a) Regn ut linjeintegralet

$$\int_C xyz \, ds$$

- b) Regn ut virvlingen til det konservative kraftfeltet

$$\mathbf{F} = 2x \mathbf{i} + 2yze^{y^2} \mathbf{j} + e^{y^2} \mathbf{k}$$

Begrunn at feltet konservativt.

- c) En partikkel som beveger seg langs kurven C er under påvirkning av kraftfeltet \mathbf{F} . Bestem arbeidet

$$\int_C \mathbf{F} \cdot d\mathbf{r}$$

Oppgave 4 Et vektorfelt er gitt ved

$$\mathbf{F} = (2x + 3x^2y^2 + e^{z \sin y}) \mathbf{i} + (x \sin z - 2xy^3) \mathbf{j} + z \mathbf{k}$$

Flaten S er den delen av paraboloiden

$$z = x^2 + y^2$$

hvor $z \leq 4$. D er regionen i rommet avgrenset nedad av S og oppad av planet $z = 4$.

- a) Regn ut divergensen til \mathbf{F} . Tegn en skisse og beskriv regionen D i passende koordinater. Bruk dette til å regne ut trippelintegralet

$$\iiint_D \nabla \cdot \mathbf{F} \, dV$$

- b) Bruk divergensteoremet til å bestemme fluksen av \mathbf{F} gjennom flaten S :

$$\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$$

Enhetsnormalvektoren peker vekk fra z -aksen, altså $\mathbf{n} \cdot (x \mathbf{i} + y \mathbf{j}) \geq 0$.

Hint: merk at S bare er en del av randflaten til D .

Oppgave 5 En kloss med masse m er koblet til en fjær. Bevegelsen er rettlinjet og klossens posisjon ved tidspunktet t er $x(t)$. Kreftene som virker på klossen er fjærkraften $F_k = -kx$ og luftmotstanden $F_b = -b\frac{dx}{dt}$, hvor k og b er to konstanter.

- a) i) Bruk Newton's andre lov til å skrive ned en andreordens bevegelsesligning for kloss-fjær systemet.
- ii) Skriv bevegelsesligningene om på dimensjonsløs form ved å innføre dimensjonsløse variable \tilde{t} og \tilde{x} definert

$$t = \tau \cdot \tilde{t}, \quad x = L \cdot \tilde{x},$$

hvor τ er en tidsskala med SI-enhet s (sekund) og L er en lengdeskala med SI-enhet m (meter). Vis at ligningen kan skrives på formen

$$\frac{d^2\tilde{x}}{d\tilde{t}^2} + \alpha \frac{d\tilde{x}}{d\tilde{t}} + \tilde{x} = 0$$

ved å velge en passende tidsskala τ . Skriv ned et uttrykk for α .

I oppgave b) og c) antar vi at $m = 1$ kg, $k = \frac{1}{4}$ N/m og $b = 1$ Ns/m.

- b) i) Bestem verdien til konstanten α og vis at den er dimensjonsløs. Vis at bevegelsesligningen i oppg. a) ii) kan skrives om til to koblede førsteordens differensielligner for variablene \tilde{x} og $\tilde{v} = \frac{d\tilde{x}}{d\tilde{t}}$:

$$\begin{aligned} \textbf{I. } \frac{d\tilde{x}}{d\tilde{t}} &= \tilde{v}, \\ \textbf{II. } \frac{d\tilde{v}}{d\tilde{t}} &= -\tilde{x} - 2\tilde{v} \end{aligned}$$

- ii) La \tilde{x}_n og \tilde{v}_n være numeriske tilnærninger til $\tilde{x}(\tilde{t}_n)$ og $\tilde{v}(\tilde{t}_n)$, hvor $\tilde{t}_n = n \cdot \Delta\tilde{t}$. Bruk Eulers metode til å uttrykke \tilde{x}_1 og \tilde{v}_1 ved initialbetingelsene \tilde{x}_0 og \tilde{v}_0 . Ved å sette $\tilde{x}_0 = 0$ og $\tilde{v}_0 = 1$ i resultatet skal du få følgende uttrykk:

$$\begin{aligned} \tilde{x}_1 &= \Delta\tilde{t}, \\ \tilde{v}_1 &= 1 - 2\Delta\tilde{t} \end{aligned}$$

- c) Med de antatte verdiene for m , k og b har differensielligningen følgende eksakte løsning:

$$\tilde{x}(\tilde{t}) = Ae^{-\tilde{t}} + B\tilde{t}e^{-\tilde{t}}$$

Anta initialbetingelser $\tilde{x}_0 = 0$ og $\tilde{v}_0 = 1$ og sammenlign den eksakte løsningen i tidspunktet $\tilde{t} = \Delta\tilde{t}$ med uttrykket for \tilde{x}_1 og \tilde{v}_1 i oppg. b) ii). Stemmer resultatene dine med at Eulers metode er en første-ordens numerisk metode?

Vi minner om Taylor-rekken til e^x i punktet $x = 0$:

$$e^x = \sum_{n=0}^{\infty} \frac{x^n}{n!} = 1 + x + \dots$$

Collection of formulas – Matematikk 3 (IRF30017)

Conic sections

Conic sections on standard form with foci on the x -axis:

$$\text{Ellipse: } \frac{x^2}{a^2} + \frac{y^2}{b^2} = 1, \quad a > b, \quad \text{foci: } (\pm c, 0), \quad c = \sqrt{a^2 - b^2}.$$

$$\text{Hyperbola: } \frac{x^2}{a^2} - \frac{y^2}{b^2} = 1, \quad \text{foci: } (\pm c, 0), \quad c = \sqrt{a^2 + b^2}, \quad \text{asymptotes: } y = \pm(b/a)x.$$

$$\text{Parabola: } y = \frac{x^2}{4p}, \quad \text{focus: } (0, p), \quad \text{directrix: } y = -p.$$

In the case of the ellipse, a is called the *semimajor axis* and b the *semiminor axis*.

English – norwegian: conic section – kjeglesnitt, directrix – styrelinje, semimajor axis – store halvakse, semiminor axis – lille halvakse.

The method of Lagrange multipliers

Assume that $f(x_1, \dots, x_n)$ and $g(x_1, \dots, x_n)$ are differentiable functions and that $\nabla g \neq 0$ when $g = 0$. The stationary points of f subject to the constraint $g = 0$ are found by solving the $n + 1$ scalar equations

$$\nabla f = \lambda \nabla g, \quad g = 0$$

for the $n + 1$ unknowns λ, x_1, \dots, x_n . The stationary points are *candidates* for local maxima and minima of f subject to $g = 0$.

Double and triple integrals

Cartesian (x, y, z) , **cylindrical** (r, θ, z) and **spherical** (ρ, ϕ, θ) coordinates of a point P :

$$\text{From cylindrical to Cartesian: } x = r \cos \theta, \quad y = r \sin \theta, \quad z = z.$$

$$\text{From spherical to cylindrical: } r = \rho \sin \phi, \quad \theta = \theta, \quad z = \rho \cos \phi.$$

$$\text{From spherical to Cartesian: } x = \rho \sin \phi \cos \theta, \quad y = \rho \sin \phi \sin \theta, \quad z = \rho \cos \phi.$$

$r = \sqrt{x^2 + y^2}$ is the distance to the z axis and $\rho = \sqrt{x^2 + y^2 + z^2}$ is the distance to the origin ($|\overrightarrow{OP}|$). $\theta \in [0, 2\pi]$ is the polar angular coordinate of the projection of P on the xy -plane and $\phi \in [0, \pi]$ is the angle between the z -axis and \overrightarrow{OP} .

Area and volume elements:

$$dA = dx dy = r dr d\theta = |J(u, v)| du dv,$$

$$dV = dx dy dz = r dz dr d\theta = \rho^2 \sin \phi d\rho d\phi d\theta = |J(u, v, w)| du dv dw,$$

$$J(u, v) = \frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix}, \quad J(u, v, w) = \frac{\partial(x, y, z)}{\partial(u, v, w)}$$

Applications of double and triple integrals:

$$\text{Area of } R : A = \iint_R dA,$$

$$\text{Volume of } D : V = \iiint_D dV$$

$$\text{Average of } f \text{ over } R : \bar{f} = \frac{1}{A} \iint_R f(x, y) dA, \quad \text{Average of } f \text{ over } D : \bar{f} = \frac{1}{V} \iiint_D f(x, y, z) dV$$

Object with mass density $\delta(x, y, z)$ occupying a region D in space:

$$\text{Mass: } M = \iiint_D \delta(x, y, z) dV, \quad \text{Center of mass: } \bar{x} = \frac{M_{yz}}{M}, \quad \bar{y} = \frac{M_{xz}}{M}, \quad \bar{z} = \frac{M_{xy}}{M},$$

$$M_{yz} = \iiint_D x \delta(x, y, z) dV, \quad M_{xz} = \iiint_D y \delta(x, y, z) dV, \quad M_{xy} = \iiint_D z \delta(x, y, z) dV$$

Parametric curves and line integrals

Below the following parametrization of a curve C in space is assumed:

$$C : \quad \mathbf{r}(t) = g(t)\mathbf{i} + h(t)\mathbf{j} + k(t)\mathbf{k}, \quad a \leq t \leq b$$

Tangent vector: $\mathbf{v}(t) = \frac{d\mathbf{r}}{dt} = g'(t)\mathbf{i} + h'(t)\mathbf{j} + k'(t)\mathbf{k}$, Unit tangent vector: $\mathbf{T} = \frac{\mathbf{v}}{|\mathbf{v}|}$, $|\mathbf{v}| = \sqrt{\mathbf{v} \cdot \mathbf{v}}$,

Arc length: $L = \int_a^b |\mathbf{v}| dt$, Arc length parameter: $s(t) = \int_a^t |\mathbf{v}(t')| dt'$

Relations between differentials:

$$d\mathbf{r} = dx\mathbf{i} + dy\mathbf{j} + dz\mathbf{k}, \quad d\mathbf{r} = \mathbf{T}ds, \quad ds = |\mathbf{v}|dt$$

Line integral of scalar $f(x, y, z)$ along C :

$$\int_C f(x, y, z) ds = \int_a^b f(\mathbf{r}(t)) |\mathbf{v}(t)| dt, \quad f(\mathbf{r}(t)) = f(g(t), h(t), k(t))$$

Line integral of vector field $\mathbf{F}(x, y, z) = M(x, y, z)\mathbf{i} + N(x, y, z)\mathbf{j} + P(x, y, z)\mathbf{k}$ along C :

$$\overbrace{\int_C \mathbf{F} \cdot \mathbf{T} ds = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C M dx + N dy + P dz}^{\text{definitions}} = \overbrace{\int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{v} dt}^{\text{how to calculate}}$$

The line integral of the x -component of \mathbf{F} along C :

$$\int_C M(x, y, z) dx = \int_a^b M(\mathbf{r}(t)) \frac{dx}{dt} dt = \int_a^b M(g(t), h(t), k(t)) g'(t) dt$$

English – norwegian: line integral – linjeintegral, unit tangent vektor – enhets-tangentvektor, arc length – buelengde.

Names on line integrals: work, flow, circulation and flux

Let \mathbf{F} be a vector field in \mathbb{R}^n and C a parametrized curve in the same space. The line integral

$$\int_C \mathbf{F} \cdot d\mathbf{r}$$

is called the

- *work* done by \mathbf{F} on an object moving along the curve C if \mathbf{F} is a force field
- *flow* of \mathbf{F} along C if \mathbf{F} is a velocity field
- *circulation* of \mathbf{F} along C if \mathbf{F} is a velocity field and C is a closed curve
(for a closed curve the line integral is often written \oint_C)

Flux integral in two dimensions: Let $\mathbf{F} = M\mathbf{i} + N\mathbf{j}$ be a vector field and C a simple closed curve in the plane (\mathbb{R}^2) with unit normal \mathbf{n} oriented outwards. The following line integral is the flux of \mathbf{F} across the curve C :

$$\text{flux} = \oint_C \mathbf{F} \cdot \mathbf{n} ds = \oint_C M dy - N dx$$

Flux integral in three dimensions: see surface integrals below.

English – norwegian: work – arbeid, flow – strøm, circulation – sirkulasjon, flux – fluks.

del, divergence and curl

Del operator:

$$\mathbb{R}^3 : \quad \nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z}, \quad \mathbb{R}^n : \quad \nabla = \sum_{i=1}^n \mathbf{e}_i \frac{\partial}{\partial x^i}$$

The following definitions assume that $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ is a vector field in space (\mathbb{R}^3), but the divergence generalizes naturally to a space of arbitrary dimensions (\mathbb{R}^n):

$$\text{Divergence of } \mathbf{F} : \quad \text{div } \mathbf{F} = \nabla \cdot \mathbf{F} = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z}, \quad \text{Curl of } \mathbf{F} : \quad \text{curl } \mathbf{F} = \nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & P \end{vmatrix}$$

Identities: $\nabla \times (\nabla f) = 0$, $\nabla \cdot (\nabla \times \mathbf{F}) = 0$

English – norwegian: del – nabla, divergence – divergens, curl – virvling.

Conservative fields and path independence

The following statements are equivalent if \mathbf{F} is a vector field in space whose components have continuous partial derivatives in a connected and simply connected domain D and C is a curve in the same domain:

1. \mathbf{F} is conservative
(this is another way to say that the integral $\int_C \mathbf{F} \cdot d\mathbf{r}$ is path independent)
2. \mathbf{F} is curl-free, $\nabla \times \mathbf{F} = \mathbf{0}$
(this provides a component test for conservative fields, in the plane write $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + 0\mathbf{k}$)
3. \mathbf{F} is a gradient field: $\mathbf{F} = \nabla f$
(the function $f(x, y, z)$ is called a *potential function* for \mathbf{F})
4. $\int_A^B \mathbf{F} \cdot d\mathbf{r} = f(B) - f(A)$ for all curves C from A to B
5. $\oint_C \mathbf{F} \cdot d\mathbf{r} = 0$ for all closed curves C

English – norwegian: conservative – konservativ, path independent – veiuavhengig, curl-free – virvelfri.

Green's theorem

Let R be a region in the plane bounded by the piecewise smooth, simple closed curve C and let $\mathbf{F} = M(x, y)\mathbf{i} + N(x, y)\mathbf{j} + 0\mathbf{k}$ be a vector field with components M and N that have continuous partial derivatives.

Circulation-curl form:

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_R \nabla \times \mathbf{F} \cdot \mathbf{k} dA$$

or

$$\oint_C M dx + N dy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy$$

Flux-divergence form:

$$\oint_C \mathbf{F} \cdot \mathbf{n} ds = \iint_R \nabla \cdot \mathbf{F} dA$$

or

$$\oint_C M dy - N dx = \iint_R \left(\frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} \right) dx dy$$

English – norwegian: piecewise smooth – stykkevis glatt, simple curve – enkel kurve.

Surface integrals

Let S be a smooth surface in space (\mathbb{R}^3). The area element $d\sigma$ depends on the description of S :

- 1) $d\sigma = |\mathbf{r}_u \times \mathbf{r}_v| du dv$ if S is given **parametrically** as $\mathbf{r}(u, v) = f_1(u, v)\mathbf{i} + f_2(u, v)\mathbf{j} + f_3(u, v)\mathbf{k}$
- 2) $d\sigma = \frac{|\nabla G|}{|\nabla G \cdot \mathbf{k}|} dx dy$ if S is given **implicitly** by the equation $G(x, y, z) = 0$
- 3) $d\sigma = \sqrt{g_x^2 + g_y^2 + 1} dx dy$ if S is given **explicitly** as the graph $z = g(x, y)$

Below the case 3) of an explicitly defined surface is assumed. Let R be the shadow of S on the xy -plane. The area of S is:

$$A = \iint_S d\sigma = \iint_R \sqrt{g_x^2 + g_y^2 + 1} dx dy$$

The integral of a scalar $f(x, y, z)$ over S :

$$\iint_S f(x, y, z) d\sigma = \iint_R f(x, y, g(x, y)) \sqrt{g_x^2 + g_y^2 + 1} dx dy$$

A surface has two unit normal fields:

$$\mathbf{n} = \pm \frac{\nabla G}{|\nabla G|} = \pm \frac{-g_x \mathbf{i} - g_y \mathbf{j} + \mathbf{k}}{\sqrt{g_x^2 + g_y^2 + 1}}$$

For a given choice of \mathbf{n} the *flux* of $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ across S is:

$$\text{Flux} = \iint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \text{sgn}(\mathbf{n} \cdot \mathbf{k}) \iint_R -Mg_x - Ng_y + P dx dy$$

English – norwegian: surface integral – flateintegral, unit normal – enhetsnormal.

Stoke's theorem and the divergence theorem

Let S be an oriented piecewise smooth surface in space having a piecewise smooth boundary curve C that is directed counterclockwise relative to the unit normal field \mathbf{n} of S . Stokes theorem:

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma$$

Let D be a region in space with a piecewise smooth boundary surface S having an outward unit normal field \mathbf{n} . Divergence theorem:

$$\iint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \iiint_D \nabla \cdot \mathbf{F} dV$$

In both theorems the components of $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ have continuous partial derivatives.

English – norwegian: boundary – rand, boundary curve – randkurve, boundary surface – randflate, outward unit normal – utoverrettet enhetsnormal.

Modeling in physics

Numerical methods

Consider the first-order differential equation:

$$\frac{du}{dt} = f(u, t)$$

Let u_n be a numerical approximation to $u(t_n)$, where $t_n = t_0 + n\Delta t$.

Euler method: Use the tangent at the previous point to estimate the next:

$$u_{n+1} = u_n + \left(\frac{du}{dt} \right)_n \Delta t = u_n + f(u_n, t_n) \Delta t$$

Or more compactly:

$$u_{n+1} = u_n + f_n \Delta t$$

First order method (local error: $\sim \Delta t^2$, global error: $\sim \Delta t$).

Midpoint method: Use Euler's method with a half time step to estimate the slope at the midpoint (trial step), then apply this to estimate the next point:

$$\begin{aligned} u_{n+\frac{1}{2}} &= u_n + \left(\frac{du}{dt} \right)_n \frac{\Delta t}{2} = u_n + \frac{1}{2} f(u_n, t_n) \Delta t, \quad (\text{trial step}), \\ u_{n+1} &= u_n + \left(\frac{du}{dt} \right)_{n+\frac{1}{2}} \Delta t = u_n + f(u_{n+\frac{1}{2}}, t_n + \frac{\Delta t}{2}) \Delta t \end{aligned}$$

Or more compactly:

$$\begin{aligned} u_{n+\frac{1}{2}} &= u_n + \frac{1}{2} f_n \Delta t, \quad (\text{trial step}), \\ u_{n+1} &= u_n + f_{n+\frac{1}{2}} \Delta t \end{aligned}$$

Second order method (local error: $\sim \Delta t^3$, global error: $\sim \Delta t^2$).

Higher order differential equations

A second order differential equation can be rewritten as a system of two coupled first order equations:

$$\begin{aligned} \frac{d^2u}{dt^2} = f \left(u, \frac{du}{dt}, t \right) &\iff \text{I. } \frac{du}{dt} = v, \\ &\quad \text{II. } \frac{dv}{dt} = f(u, v, t) \end{aligned}$$

The numerical schemes above can then be applied to find u_{n+1} and v_{n+1} from u_n and v_n .

Dimensionless variables

An ordinary differential equation for $x(t)$ can be written on dimensionless form by introducing a length scale L and time scale τ :

$$x = L\tilde{x}, \quad t = \tau\tilde{t} \quad \rightarrow \quad \frac{dx}{dt} = \frac{L}{\tau} \frac{d\tilde{x}}{d\tilde{t}}, \quad \frac{d^2x}{dt^2} = \frac{L}{\tau^2} \frac{d^2\tilde{x}}{d\tilde{t}^2},$$

where in SI units $\text{Dim}(x) = \text{Dim}(L) = \text{m}$, $\text{Dim}(t) = \text{Dim}(\tau) = \text{s}$ and $\text{Dim}(\tilde{x}) = \text{Dim}(\tilde{t}) = 1$.

SI base units: m, s, kg. SI derived units: N=kg·ms⁻² (Newton's 2nd law), J=N·m (work-energy theorem).

Some solutions of selected differential equations

Harmonic oscillator equation (ordinary, linear, homogeneous):

$$\frac{d^2x}{dt^2} + w^2 x = 0 \quad \rightarrow \quad x(t) = A \cos(wt + \phi)$$

Amplitude: A [m], angular frequency: w [rad/s], frequency: $f = \frac{w}{2\pi}$ [Hz], period: $T = \frac{1}{f} = \frac{2\pi}{w}$, phase: ϕ [rad].

One-dimensional wave equation (partial, linear, homogeneous):

$$\frac{1}{v^2} \frac{\partial^2 y}{\partial t^2} = \frac{\partial^2 y}{\partial x^2}$$

Mechanical waves on a string:

- Harmonic wave travelling to the right: $y(x, t) = A \cos(kx - wt + \phi)$, $w = v \cdot k$.
Wave number: k [m^{-1}], wave length: $\lambda = \frac{2\pi}{k}$ [m].
- Standing waves with boundary conditions $y(0, t) = y(L, t) = 0$:
 $y(x, t) = A \sin(kx) \cdot \cos(wt)$, $w = v \cdot k$, $k = \frac{n\pi}{L}$, $n = 1, 2, 3, \dots$

One-dimensional heat equation / diffusion equation (partial, linear, homogeneous):

$$\frac{\partial u}{\partial t} = c^2 \frac{\partial^2 u}{\partial x^2} \quad \rightarrow \quad u(x, t) = A \sin(kx) \cdot e^{-(ck)^2 t}, \quad k = \frac{n\pi}{L}, \quad n = 1, 2, 3, \dots$$

The solutions above satisfy the boundary conditions $u(0, t) = u(L, t) = 0$.

From previous courses

Scalar product and vector product

When $\mathbf{a} = a_1\mathbf{i} + a_2\mathbf{j} + a_3\mathbf{k}$ and $\mathbf{b} = b_1\mathbf{i} + b_2\mathbf{j} + b_3\mathbf{k}$:

$$\mathbf{a} \cdot \mathbf{b} = |\mathbf{a}| \cdot |\mathbf{b}| \cos \alpha = a_1b_1 + a_2b_2 + a_3b_3, \quad \mathbf{a} \times \mathbf{b} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix}, \quad |\mathbf{a} \times \mathbf{b}| = |\mathbf{a}| \cdot |\mathbf{b}| \sin \alpha$$

Straight line in space

Parametrization of a line through the point $P_0(x_0, y_0, z_0)$ parallel to $\vec{v} = [a, b, c]$:

$$\mathbf{r}(t) = \mathbf{r}_0 + t\mathbf{v} = (x_0 + at)\mathbf{i} + (y_0 + bt)\mathbf{j} + (z_0 + ct)\mathbf{k}, \quad -\infty \leq t \leq \infty$$

A possible parametrization of a straight line from \mathbf{r}_1 to \mathbf{r}_2 :

$$\mathbf{r}(t) = \mathbf{r}_1 + (\mathbf{r}_2 - \mathbf{r}_1)t, \quad 0 \leq t \leq 1$$

Plane in space

Equation for a plane through the point $P_0(x_0, y_0, z_0)$ normal to $\vec{n} = [a, b, c]$:

$$\overrightarrow{P_0P} \cdot \vec{n} = 0 \quad \rightarrow \quad (x - x_0)a + (y - y_0)b + (z - z_0)c = 0$$

Circle in the plane

Equation for a circle with radius a and center in (x_0, y_0) : $(x - x_0)^2 + (y - y_0)^2 = a^2$

Taylor expansion

Taylor series of a function $f(x)$ about the point $x = a$:

$$f(x) = \sum_{k=0}^{\infty} \frac{f^{(k)}(a)}{k!} (x - a)^k = f(a) + f'(a)(x - a) + \frac{1}{2!} f''(a)(x - a)^2 + \dots$$

Taylor polynom of degree n :

$$P_n(x) = \sum_{k=0}^n \frac{f^{(k)}(a)}{k!} (x - a)^k = f(a) + f'(a)(x - a) + \frac{1}{2!} f''(a)(x - a)^2 + \dots + \frac{f^{(n)}(a)}{n!} (x - a)^n$$

Linear approximation to $f(x)$ around $x = a$:

$$f(x) \simeq f(a) + f'(a)(x - a) \quad \text{if} \quad \left| \frac{1}{2} f''(a)(x - a)^2 \right| \ll |f'(a)(x - a)|$$

Some trigonometric identities

$$\begin{aligned} \sin^2 u + \cos^2 u &= 1, & \sin(u + v) &= \sin u \cos v + \cos u \sin v, & \cos(u + v) &= \cos u \cos v - \sin u \sin v, \\ \sin(2u) &= 2 \sin u \cos u, & \cos(2u) &= \cos^2 u - \sin^2 u, & \cos^2 u &= (1 + \cos(2u))/2, & \sin^2 u &= (1 - \cos(2u))/2 \end{aligned}$$