

EKSAMEN

Emnekode: IRF30017	Emnenavn: Matematikk 3
Dato: 24.04.2019 Sensurfrist: 15.05.2019	Eksamenstid: 0900-1300
Antall oppgavesider: 3 Antall vedleggsider: 7	Faglærer: Fredrikstad: Mikjel Thorsrud (41 51 86 10) Halden: Einar von Krogh (69 60 82 99) Oppgaven er kontrollert: Ja
Hjelpemidler: <ul style="list-style-type: none">• Godkjent kalkulator• Ett A4-ark med valgfritt innhold (maskin eller håndskrevet, kan skrive på begge sider)• Enten Tor Andersen: "Aktiv formelsamling i matematikk" eller "Gyldendals formelsamling i matematikk"	
Om eksamensoppgaven: <p>Oppgavesettet består av 11 deloppgaver som i utgangspunktet vektes likt: 1a, 1b, 1c, 2a, 2b, 2c, 2d, 2e, 3a, 3b, 3c. Formelsamling (7 sider) er vedlagt.</p>	
Kandidaten må selv kontrollere at oppgavesettet er fullstendig	



Oppgave 1

- a) Regn ut trippelintegralet

$$\int_0^{2\pi} \int_0^{\pi/2} \int_0^3 \rho^2 \sin \phi \, d\rho \, d\phi \, d\theta$$

Vis alle mellomregninger. Integralet gir volumet til et objekt i rommet. Hva slags objekt?

- b) R er området i planet avgrenset av linjene $y = x$, $y = 6 - 2x$ og y -aksen. Tegn en skisse av R og regn ut dobbeltintegralet

$$\iint_R 3xy \, dA$$

- c) D er området i første oktant (der $x \geq 0$, $y \geq 0$, $z \geq 0$) som er avgrenset av planet $x + 2y + z = 4$ og koordinatplanene.

- i) Tegn en skisse av området D . Bestem volumet til D på valgfri måte (det er ok å bruke kjente volumformler).
- ii) Et legeme som okkuperer området D har innvendig temperatur gitt ved funksjonen $T(x, y, z) = 20 + z$. Skriv ned et beregningsklart trippelintegral som gir gjennomsnittstemperaturen \bar{T} til legemet. Du trenger ikke regne ut integralet, men det skal kunne tastes direkte inn på en kalkulator og gi svaret $\bar{T} = 21$.

Oppgave 2

- a) En ellipse er bestemt av ligningen

$$x^2 + 4y^2 = 16.$$

Skriv ligningen på standardform og bestem store og lille halvakse. Bestem koordinatene til brennpunktene.

- b) En kurve C har følgende parametrisering:

$$\mathbf{r}(t) = 4 \cos \pi t \mathbf{i} + 2 \sin \pi t \mathbf{j}, \quad 0 \leq t \leq 2.$$

- i) Vis ved innsetting i ligningen for ellipsen at kurven C er ellipsen i oppg. a).
- ii) La A være punktet på ellipsen som tilsvarer parameterverdien $t = 1/6$. Skriv ned de kartesiske koordinatene (x, y) til punktet A .
- c) i) La $\mathbf{v}(t) = \frac{d\mathbf{r}}{dt}$ være tangentvektor til kurven C definert over. Regn ut enhets-tangentvektor $\mathbf{T}(t) = \frac{\mathbf{v}}{|\mathbf{v}|}$ i punktet A , altså $\mathbf{T}(1/6)$.
- ii) Tegn en skisse av kurven C (ellipsen). Marker punktet A og tegn inn enhets-tangentvektoren i dette punktet. Marker også brennpunktene til ellipsen.
- d) Et vektorfelt i rommet er definert ved

$$\mathbf{F}(x, y, z) = -ye^{2z} \mathbf{i} + (x + yz) \mathbf{j} + z \mathbf{k}$$

Regn ut divergensen og virvlingen til \mathbf{F} . Er vektorfeltet konservativt?

- e) Flaten S er øvre halvdel ($z \geq 0$) av ellipsoiden

$$\frac{x^2}{4^2} + \frac{y^2}{2^2} + \frac{z^2}{3^2} = 1$$

Bruk Stokes' teorem til å regne ut flateintegralet

$$\iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma$$

hvor \mathbf{F} er vektorfeltet definert over og \mathbf{n} er enhets-normalvektor til S og peker "oppover" ($\mathbf{n} \cdot \mathbf{k} \geq 0$).

Oppgave 3 En nyttårsrakett med masse m går tom for krutt mens den er på vei rett oppover. Kreftene som virker på raketten er da tyngdekraften og luftmotstand som begge virker i retning rett nedover. Tyngdekraften har størrelse mg , hvor g er tyngdeakselerasjonen. Vi antar en kvadratisk modell for luftmotstanden med størrelse bv^2 , hvor $v = \frac{dy}{dt}$ er raketts hastighet og b er en positiv koeffisient.

- a) i) Skriv ned en andre-ordens differensialligning for posisjonen $y(t)$ ved å bruke Newtons andre lov.
 ii) Vi innfører dimensjonsløse variable \tilde{t} og \tilde{y} definert

$$t = \tau \cdot \tilde{t}, \quad y = L \cdot \tilde{y},$$

hvor τ er en tidsskala med SI-enhet s (sekund) og L er en lengdeskala med SI-enhet m (meter). Vis at differensialligningen kan skrives på dimensjonsløs form som

$$\frac{d^2\tilde{y}}{d\tilde{t}^2} + \left(\frac{d\tilde{y}}{d\tilde{t}}\right)^2 + 1 = 0.$$

Bestem τ og L uttrykt ved b , m og g .

- b) Ved tidspunktet $\tilde{t} = 0$ er posisjonen $\tilde{y}_0 = 1$ og hastigheten $\tilde{v}_0 = 1$. Bruk midtpunktmetoden til å finne en tilnærmet verdi for posisjonen \tilde{y} ved tidspunktet $\tilde{t} = 0.1$. Bruk kun ett tidssteg, dvs. regn ut \tilde{y}_1 ved å bruke tidssteget $\Delta\tilde{t} = 0.1$.
 Tips: merk at vi i denne og den neste deloppgaven jobber utelukkende med de dimensjonsløse størrelsene. Ta derfor utgangspunkt i den dimensjonsløse differensialligningen skrevet ned i oppg. a). Begynn som vanlig med å skrive differensialligningen om til to koblede første-ordens ligninger for variablene \tilde{y} og \tilde{v} .
- c) Differensialligningen i oppg a) har følgende eksakte løsning:

$$\tilde{y}(\tilde{t}) = A + \ln[\cos(\tilde{t} - B)]$$

hvor A og B er konstanter. Bestem A og B ved å bruke initialbetingelsene i oppg. b). Regn ut feilen $|\tilde{y}(0.1) - \tilde{y}_1|$ til tilnærmingen i oppg. b). Stemmer feilens størrelse med at midtpunktmetoden er en andre-ordens numerisk metode?

Collection of formulas – Matematikk 3 (IRF30017)

Conic sections

Conic sections on standard form with foci on the x -axis:

$$\text{Ellipse: } \frac{x^2}{a^2} + \frac{y^2}{b^2} = 1, \quad a > b, \quad \text{foci: } (\pm c, 0), \quad c = \sqrt{a^2 - b^2}.$$

$$\text{Hyperbola: } \frac{x^2}{a^2} - \frac{y^2}{b^2} = 1, \quad \text{foci: } (\pm c, 0), \quad c = \sqrt{a^2 + b^2}, \quad \text{asymptotes: } y = \pm(b/a)x.$$

$$\text{Parabola: } y = \frac{x^2}{4p}, \quad \text{focus: } (0, p), \quad \text{directrix: } y = -p.$$

In the case of the ellipse, a is called the *semimajor axis* and b the *semiminor axis*.

English – norwegian: conic section – kjeglesnitt, directrix – styrelinje, semimajor axis – store halvakse, semiminor axis – lille halvakse.

The method of Lagrange multipliers

Assume that $f(x_1, \dots, x_n)$ and $g(x_1, \dots, x_n)$ are differentiable functions and that $\nabla g \neq 0$ when $g = 0$. The stationary points of f subject to the constraint $g = 0$ are found by solving the $n + 1$ scalar equations

$$\nabla f = \lambda \nabla g, \quad g = 0$$

for the $n + 1$ unknowns λ, x_1, \dots, x_n . The stationary points are *candidates* for local maxima and minima of f subject to $g = 0$.

Double and triple integrals

Cartesian (x, y, z) , **cylindrical** (r, θ, z) and **spherical** (ρ, ϕ, θ) coordinates of a point P :

$$\text{From cylindrical to Cartesian: } x = r \cos \theta, \quad y = r \sin \theta, \quad z = z.$$

$$\text{From spherical to cylindrical: } r = \rho \sin \phi, \quad \theta = \theta, \quad z = \rho \cos \phi.$$

$$\text{From spherical to Cartesian: } x = \rho \sin \phi \cos \theta, \quad y = \rho \sin \phi \sin \theta, \quad z = \rho \cos \phi.$$

$r = \sqrt{x^2 + y^2}$ is the distance to the z axis and $\rho = \sqrt{x^2 + y^2 + z^2}$ is the distance to the origin ($|\overrightarrow{OP}|$). $\theta \in [0, 2\pi]$ is the polar angular coordinate of the projection of P on the xy -plane and $\phi \in [0, \pi]$ is the angle between the z -axis and \overrightarrow{OP} .

Area and volume elements:

$$dA = dx dy = r dr d\theta = |J(u, v)| du dv,$$

$$dV = dx dy dz = r dz dr d\theta = \rho^2 \sin \phi d\rho d\phi d\theta = |J(u, v, w)| du dv dw,$$

$$J(u, v) = \frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix}, \quad J(u, v, w) = \frac{\partial(x, y, z)}{\partial(u, v, w)}$$

Applications of double and triple integrals:

$$\text{Area of } R: \quad A = \iint_R dA, \quad \text{Volume of } D: \quad V = \iiint_D dV$$

$$\text{Average of } f \text{ over } R: \quad \bar{f} = \frac{1}{A} \iint_R f(x, y) dA, \quad \text{Average of } f \text{ over } D: \quad \bar{f} = \frac{1}{V} \iiint_D f(x, y, z) dV$$

Object with mass density $\delta(x, y, z)$ occupying a region D in space:

$$\text{Mass: } M = \iiint_D \delta(x, y, z) dV, \quad \text{Center of mass: } \bar{x} = \frac{M_{yz}}{M}, \quad \bar{y} = \frac{M_{xz}}{M}, \quad \bar{z} = \frac{M_{xy}}{M},$$

$$M_{yz} = \iiint_D x \delta(x, y, z) dV, \quad M_{xz} = \iiint_D y \delta(x, y, z) dV, \quad M_{xy} = \iiint_D z \delta(x, y, z) dV$$

Parametric curves and line integrals

Below the following parametrization of a curve C in space is assumed:

$$C: \quad \mathbf{r}(t) = g(t)\mathbf{i} + h(t)\mathbf{j} + k(t)\mathbf{k}, \quad a \leq t \leq b$$

$$\text{Tangent vector: } \mathbf{v}(t) = \frac{d\mathbf{r}}{dt} = g'(t)\mathbf{i} + h'(t)\mathbf{j} + k'(t)\mathbf{k}, \quad \text{Unit tangent vector: } \mathbf{T} = \frac{\mathbf{v}}{|\mathbf{v}|}, \quad |\mathbf{v}| = \sqrt{\mathbf{v} \cdot \mathbf{v}},$$

$$\text{Arc length: } L = \int_a^b |\mathbf{v}| dt, \quad \text{Arc length parameter: } s(t) = \int_a^t |\mathbf{v}(t')| dt'$$

Relations between differentials:

$$d\mathbf{r} = dx\mathbf{i} + dy\mathbf{j} + dz\mathbf{k}, \quad d\mathbf{r} = \mathbf{T}ds, \quad ds = |\mathbf{v}|dt$$

Line integral of scalar $f(x, y, z)$ along C :

$$\int_C f(x, y, z) ds = \int_a^b f(\mathbf{r}(t)) |\mathbf{v}(t)| dt, \quad f(\mathbf{r}(t)) = f(g(t), h(t), k(t))$$

Line integral of vector field $\mathbf{F}(x, y, z) = M(x, y, z)\mathbf{i} + N(x, y, z)\mathbf{j} + P(x, y, z)\mathbf{k}$ along C :

$$\int_C \mathbf{F} \cdot \mathbf{T} ds = \overbrace{\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C Mdx + Ndy + Pdz}^{\text{definitions}} = \overbrace{\int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{v} dt}^{\text{how to calculate}}$$

The line integral of the x -component of \mathbf{F} along C :

$$\int_C M(x, y, z) dx = \int_a^b M(\mathbf{r}(t)) \frac{dx}{dt} dt = \int_a^b M(g(t), h(t), k(t)) g'(t) dt$$

English – norwegian: line integral – linjeintegral, unit tangent vektor – enhets-tangentvektor, arc length – buelengde.

Names on line integrals: work, flow, circulation and flux

Let \mathbf{F} be a vector field in \mathbb{R}^n and C a parametrized curve in the same space. The line integral

$$\int_C \mathbf{F} \cdot d\mathbf{r}$$

is called the

- *work* done by \mathbf{F} on an object moving along the curve C if \mathbf{F} is a force field
- *flow* of \mathbf{F} along C if \mathbf{F} is a velocity field
- *circulation* of \mathbf{F} along C if \mathbf{F} is a velocity field and C is a closed curve (for a closed curve the line integral is often written \oint_C)

Flux integral in two dimensions: Let $\mathbf{F} = M\mathbf{i} + N\mathbf{j}$ be a vector field and C a simple closed curve in the plane (\mathbb{R}^2) with unit normal \mathbf{n} oriented outwards. The following line integral is the flux of \mathbf{F} across the curve C :

$$\text{flux} = \oint_C \mathbf{F} \cdot \mathbf{n} ds = \oint_C M dy - N dx$$

Flux integral in three dimensions: see surface integrals below.

English – norwegian: work – arbeid, flow – strøm, circulation – sirkulasjon, flux – fluks.

del, divergence and curl

Del operator:

$$\mathbb{R}^3 : \quad \nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z}, \quad \mathbb{R}^n : \quad \nabla = \sum_{i=1}^n \mathbf{e}_i \frac{\partial}{\partial x^i}$$

The following definitions assume that $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ is a vector field in space (\mathbb{R}^3), but the divergence generalizes naturally to a space of arbitrary dimensions (\mathbb{R}^n):

$$\text{Divergence of } \mathbf{F} : \quad \text{div } \mathbf{F} = \nabla \cdot \mathbf{F} = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z}, \quad \text{Curl of } \mathbf{F} : \quad \text{curl } \mathbf{F} = \nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & P \end{vmatrix}$$

$$\text{Identities:} \quad \nabla \times (\nabla f) = 0, \quad \nabla \cdot (\nabla \times \mathbf{F}) = 0$$

English – norwegian: del – nabla, divergence – divergens, curl – virvling.

Conservative fields and path independence

The following statements are equivalent if \mathbf{F} is a vector field in space whose components have continuous partial derivatives in a connected and simply connected domain D and C is a curve in the same domain:

1. \mathbf{F} is conservative
(this is another way to say that the integral $\int_C \mathbf{F} \cdot d\mathbf{r}$ is path independent)
2. \mathbf{F} is curl-free, $\nabla \times \mathbf{F} = \mathbf{0}$
(this provides a component test for conservative fields, in the plane write $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + 0\mathbf{k}$)
3. \mathbf{F} is a gradient field: $\mathbf{F} = \nabla f$
(the function $f(x, y, z)$ is called a *potential function* for \mathbf{F})
4. $\int_A^B \mathbf{F} \cdot d\mathbf{r} = f(B) - f(A)$ for all curves C from A to B
5. $\oint_C \mathbf{F} \cdot d\mathbf{r} = 0$ for all closed curves C

English – norwegian: conservative – konservativ, path independent – veiuavhengig, curl-free – virvelfri.

Green's theorem

Let R be a region in the plane bounded by the piecewise smooth, simple closed curve C and let $\mathbf{F} = M(x, y)\mathbf{i} + N(x, y)\mathbf{j} + 0\mathbf{k}$ be a vector field with components M and N that have continuous partial derivatives.

Circulation-curl form:

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_R \nabla \times \mathbf{F} \cdot \mathbf{k} \, dA$$

or

$$\oint_C M dx + N dy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx \, dy$$

Flux-divergence form:

$$\oint_C \mathbf{F} \cdot \mathbf{n} \, ds = \iint_R \nabla \cdot \mathbf{F} \, dA$$

or

$$\oint_C M dy - N dx = \iint_R \left(\frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} \right) dx \, dy$$

English – norwegian: piecewise smooth – stykkevis glatt, simple curve – enkel kurve.

Surface integrals

Let S be a smooth surface in space (\mathbb{R}^3). The area element $d\sigma$ depends on the description of S :

- 1) $d\sigma = |\mathbf{r}_u \times \mathbf{r}_v| du dv$ if S is given **parametrically** as $\mathbf{r}(u, v) = f_1(u, v)\mathbf{i} + f_2(u, v)\mathbf{j} + f_3(u, v)\mathbf{k}$
- 2) $d\sigma = \frac{|\nabla G|}{|\nabla G \cdot \mathbf{k}|} dx dy$ if S is given **implicitly** by the equation $G(x, y, z) = 0$
- 3) $d\sigma = \sqrt{g_x^2 + g_y^2 + 1} dx dy$ if S is given **explicitly** as the the graph $z = g(x, y)$

Below the case 3) of an explicitly defined surface is assumed. Let R be the shadow of S on the xy -plane. The area of S is:

$$A = \iint_S d\sigma = \iint_R \sqrt{g_x^2 + g_y^2 + 1} dx dy$$

The integral of a scalar $f(x, y, z)$ over S :

$$\iint_S f(x, y, z) d\sigma = \iint_R f(x, y, g(x, y)) \sqrt{g_x^2 + g_y^2 + 1} dx dy$$

A surface has two unit normal fields:

$$\mathbf{n} = \pm \frac{\nabla G}{|\nabla G|} = \pm \frac{-g_x \mathbf{i} - g_y \mathbf{j} + \mathbf{k}}{\sqrt{g_x^2 + g_y^2 + 1}}$$

For a given choice of \mathbf{n} the *flux* of $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ across S is:

$$\text{Flux} = \iint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \text{sgn}(\mathbf{n} \cdot \mathbf{k}) \iint_R -Mg_x - Ng_y + P dx dy$$

English – norwegian: surface integral – flateintegral, unit normal – enhetsnormal.

Stoke's theorem and the divergence theorem

Let S be an oriented piecewise smooth surface in space having a piecewise smooth boundary curve C that is directed counterclockwise relative to the unit normal field \mathbf{n} of S . Stokes theorem:

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma$$

Let D be a region in space with a piecewise smooth boundary surface S having an outward unit normal field \mathbf{n} . Divergence theorem:

$$\oiint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \iiint_D \nabla \cdot \mathbf{F} dV$$

In both theorems the components of $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ have continuous partial derivatives.

English – norwegian: boundary – rand, boundary curve – randkurve, boundary surface – randflate, outward unit normal – utoverrettet enhetsnormal.

Modeling in physics

Numerical methods

Consider the first-order differential equation:

$$\frac{du}{dt} = f(u, t)$$

Let u_n be a numerical approximation to $u(t_n)$, where $t_n = t_0 + n\Delta t$.

Euler method: Use the tangent at the previous point to estimate the next:

$$u_{n+1} = u_n + \left(\frac{du}{dt}\right)_n \Delta t = u_n + f(u_n, t_n)\Delta t$$

Or more compactly:

$$u_{n+1} = u_n + f_n \Delta t$$

First order method (local error: $\sim \Delta t^2$, global error: $\sim \Delta t$).

Midpoint method: Use Euler's method with a half time step to estimate the slope at the midpoint (trial step), then apply this to estimate the next point:

$$u_{n+\frac{1}{2}} = u_n + \left(\frac{du}{dt}\right)_n \frac{\Delta t}{2} = u_n + \frac{1}{2}f(u_n, t_n)\Delta t, \quad (\text{trial step}),$$
$$u_{n+1} = u_n + \left(\frac{du}{dt}\right)_{n+\frac{1}{2}} \Delta t = u_n + f(u_{n+\frac{1}{2}}, t_n + \frac{\Delta t}{2})\Delta t$$

Or more compactly:

$$u_{n+\frac{1}{2}} = u_n + \frac{1}{2}f_n \Delta t, \quad (\text{trial step}),$$
$$u_{n+1} = u_n + f_{n+\frac{1}{2}} \Delta t$$

Second order method (local error: $\sim \Delta t^3$, global error: $\sim \Delta t^2$).

Higher order differential equations

A second order differential equation can be rewritten as a system of two coupled first order equations:

$$\frac{d^2u}{dt^2} = f\left(u, \frac{du}{dt}, t\right) \iff \begin{array}{l} \text{I. } \frac{du}{dt} = v, \\ \text{II. } \frac{dv}{dt} = f(u, v, t) \end{array}$$

The numerical schemes above can then be applied to find u_{n+1} and v_{n+1} from u_n and v_n .

Dimensionless variables

An ordinary differential equation for $x(t)$ can be written on dimensionless form by introducing a length scale L and time scale τ :

$$x = L\tilde{x}, \quad t = \tau\tilde{t} \quad \longrightarrow \quad \frac{dx}{dt} = \frac{L}{\tau} \frac{d\tilde{x}}{d\tilde{t}}, \quad \frac{d^2x}{dt^2} = \frac{L}{\tau^2} \frac{d^2\tilde{x}}{d\tilde{t}^2},$$

where in SI units $\text{Dim}(x) = \text{Dim}(L) = \text{m}$, $\text{Dim}(t) = \text{Dim}(\tau) = \text{s}$ and $\text{Dim}(\tilde{x}) = \text{Dim}(\tilde{t}) = 1$.

SI base units: m, s, kg. SI derived units: $\text{N}=\text{kg}\cdot\text{m}\cdot\text{s}^{-2}$ (Newton's 2nd law), $\text{J}=\text{N}\cdot\text{m}$ (work-energy theorem).

Some solutions of selected differential equations

Harmonic oscillator equation (ordinary, linear, homogeneous):

$$\frac{d^2x}{dt^2} + w^2x = 0 \quad \rightarrow \quad x(t) = A \cos(wt + \phi)$$

Amplitude: A [m], angular frequency: w [rad/s], frequency: $f = \frac{w}{2\pi}$ [Hz], period: $T = \frac{1}{f} = \frac{2\pi}{w}$, phase: ϕ [rad].

One-dimensional wave equation (partial, linear, homogeneous):

$$\frac{1}{v^2} \frac{\partial^2 y}{\partial t^2} = \frac{\partial^2 y}{\partial x^2}$$

Mechanical waves on a string:

- Harmonic wave travelling to the right: $y(x, t) = A \cos(kx - wt + \phi)$, $w = v \cdot k$.
Wave number: k [m^{-1}], wave length: $\lambda = \frac{2\pi}{k}$ [m].
- Standing waves with boundary conditions $y(0, t) = y(L, t) = 0$:
 $y(x, t) = A \sin(kx) \cdot \cos(wt)$, $w = v \cdot k$, $k = \frac{n\pi}{L}$, $n = 1, 2, 3, \dots$

One-dimensional heat equation / diffusion equation (partial, linear, homogeneous):

$$\frac{\partial u}{\partial t} = c^2 \frac{\partial^2 u}{\partial x^2} \quad \rightarrow \quad u(x, t) = A \sin(kx) \cdot e^{-(ck)^2 t}, \quad k = \frac{n\pi}{L}, \quad n = 1, 2, 3, \dots$$

The solutions above satisfy the boundary conditions $u(0, t) = u(L, t) = 0$.

From previous courses

Scalar product and vector product

When $\mathbf{a} = a_1\mathbf{i} + a_2\mathbf{j} + a_3\mathbf{k}$ and $\mathbf{b} = b_1\mathbf{i} + b_2\mathbf{j} + b_3\mathbf{k}$:

$$\mathbf{a} \cdot \mathbf{b} = |\mathbf{a}| \cdot |\mathbf{b}| \cos \alpha = a_1b_1 + a_2b_2 + a_3b_3, \quad \mathbf{a} \times \mathbf{b} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix}, \quad |\mathbf{a} \times \mathbf{b}| = |\mathbf{a}| \cdot |\mathbf{b}| \sin \alpha$$

Straight line in space

Parametrization of a line through the point $P_0(x_0, y_0, z_0)$ parallel to $\vec{v} = [a, b, c]$:

$$\mathbf{r}(t) = \mathbf{r}_0 + t\mathbf{v} = (x_0 + at)\mathbf{i} + (y_0 + bt)\mathbf{j} + (z_0 + ct)\mathbf{k}, \quad -\infty \leq t \leq \infty$$

A possible parametrization of a straight line from \mathbf{r}_1 to \mathbf{r}_2 :

$$\mathbf{r}(t) = \mathbf{r}_1 + (\mathbf{r}_2 - \mathbf{r}_1)t, \quad 0 \leq t \leq 1$$

Plane in space

Equation for a plane through the point $P_0(x_0, y_0, z_0)$ normal to $\vec{n} = [a, b, c]$:

$$\overrightarrow{P_0P} \cdot \vec{n} = 0 \quad \rightarrow \quad (x - x_0)a + (y - y_0)b + (z - z_0)c = 0$$

Circle in the plane

Equation for a circle with radius a and center in (x_0, y_0) : $(x - x_0)^2 + (y - y_0)^2 = a^2$

Taylor expansion

Taylor series of a function $f(x)$ about the point $x = a$:

$$f(x) = \sum_{k=0}^{\infty} \frac{f^{(k)}(a)}{k!} (x - a)^k = f(a) + f'(a)(x - a) + \frac{1}{2!} f''(a)(x - a)^2 + \dots$$

Taylor polynomial of degree n :

$$P_n(x) = \sum_{k=0}^n \frac{f^{(k)}(a)}{k!} (x - a)^k = f(a) + f'(a)(x - a) + \frac{1}{2!} f''(a)(x - a)^2 + \dots + \frac{f^{(n)}(a)}{n!} (x - a)^n$$

Linear approximation to $f(x)$ around $x = a$:

$$f(x) \simeq f(a) + f'(a)(x - a) \quad \text{if} \quad \left| \frac{1}{2} f''(a)(x - a)^2 \right| \ll |f'(a)(x - a)|$$

Some trigonometric identities

$$\begin{aligned} \sin^2 u + \cos^2 u &= 1, & \sin(u + v) &= \sin u \cos v + \cos u \sin v, & \cos(u + v) &= \cos u \cos v - \sin u \sin v, \\ \sin(2u) &= 2 \sin u \cos u, & \cos(2u) &= \cos^2 u - \sin^2 u, & \cos^2 u &= (1 + \cos(2u))/2, & \sin^2 u &= (1 - \cos(2u))/2 \end{aligned}$$